

536,762

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property  
Organization  
International Bureau



(43) International Publication Date  
1 July 2004 (01.07.2004)

PCT

(10) International Publication Number  
**WO 2004/055378 A1**

(51) International Patent Classification<sup>7</sup>: **F04D 27/02,**  
19/04

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(21) International Application Number:  
PCT/GB2003/005377

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(22) International Filing Date: 9 December 2003 (09.12.2003)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
0229352.0 17 December 2002 (17.12.2002) GB

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(81) Designated States (*national*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

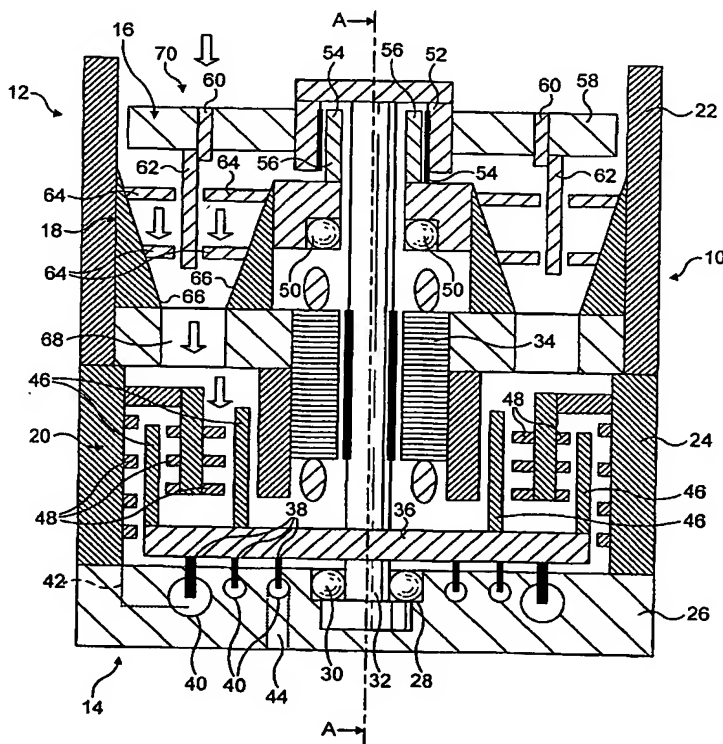
(84) Designated States (*regional*): ARIPO patent (BW, GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE,

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[Continued on next page]

(54) Title: **VACUUM PUMPING ARRANGEMENT AND METHOD OF OPERATING SAME**



(57) Abstract: A vacuum pumping arrangement (10) for controlling pressure in a chamber, the arrangement comprising a molecular pumping mechanism (12) and a backing pumping mechanism (14). The backing pumping mechanism (14) is rotatable by a motor (34), the motor being arranged to rotate the molecular pumping mechanism (12) simultaneously with the backing pumping mechanism (14). Means are provided for controlling the rotational speeds of the backing pumping mechanism and the molecular pumping mechanism.

WO 2004/055378 A1



SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

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**Published:**

— *with international search report*

## VACUUM PUMPING ARRANGEMENT AND METHOD OF OPERATING SAME

The present invention relates to a vacuum pumping arrangement and a  
5 method of controlling pressure in a chamber connected to an inlet of a vacuum  
pumping arrangement.

A known vacuum pumping arrangement for evacuating a chamber  
comprises a molecular pump which may include: molecular drag pumping  
means; or turbomolecular pumping means; or both molecular drag pumping  
10 means and turbomolecular pumping means. If both pumping means are  
included the turbomolecular pumping means are connected in series with the  
molecular drag pumping means. The pumping arrangement is capable of  
evacuating the chamber to very low pressures in the region of  $1 \times 10^{-6}$  mbar.  
The compression ratio achieved by the molecular pump is not sufficient to  
15 achieve such low pressures whilst at the same time exhausting to atmosphere  
and therefore a backing pump is provided to reduce pressure at the exhaust of  
the molecular pump and hence permit very low pressures to be achieved at the  
inlet thereof.

The turbomolecular pumping means of a molecular pump comprises a  
20 circumferential array of angled blades supported at a generally cylindrical  
rotor body. During normal operation the rotor is rotated between 20,000 and  
200,000 revolutions per minute during which time the rotor blades collide  
with molecules in a gas urging them towards the pump outlet. Normal

operation occurs therefore at molecular flow conditions at pressures of less than about 0.01 mbar. As it will be appreciated, the turbomolecular pumping means does not work effectively at high pressures, at which the angled rotor blades cause undesirable windage, or resistance to rotation of the rotor.

5           During semiconductor processing, it is often required that the pressure in the processing chamber is modified for different processing techniques and different gases used. Control of the pressure at the inlet of the molecular pump is therefore important. Hereto, a number of ways have been proposed to control inlet pressure and these include the provision of a throttle valve  
10       between the inlet and the chamber, or between the outlet of the molecular pump and the inlet of the backing pump. Although control of the speed of rotation of the molecular pump would affect inlet pressure, a typical motor used for driving the molecular pump is not sufficiently powerful to control the  
15       ~~speed of rotation quickly enough to meet the required rates of pressure change~~ and the use of a more powerful motor has not been considered practical when other less expensive methods of pressure control are available.

It is desirable to provide an improved vacuum pumping arrangement and method of controlling pressure in a chamber connected to an inlet of a vacuum pumping arrangement.

20           The present invention provides a vacuum pumping arrangement for controlling pressure in a chamber, the arrangement comprising a molecular pumping mechanism and a backing pumping mechanism, said backing pumping mechanism being rotatable by a motor, said motor being arranged to

rotate said molecular pumping mechanism simultaneously with said backing pumping mechanism, and means for controlling the rotational speeds of the backing pumping mechanism and the molecular pumping mechanism.

5 The present invention also provides a method of controlling pressure in a chamber connected to an inlet of a vacuum pumping arrangement comprising a backing pumping mechanism and a molecular pumping mechanism, and a motor for driving said backing pumping mechanism, the method comprising using said motor to control rotation of said molecular pumping mechanism thereby to control pressure in said chamber.

10 Other aspects of the present invention are defined in the accompanying claims.

In order that the present invention may be well understood, some embodiments thereof, which are given by way of example only, will now be described with reference to the accompanying drawings, in which:

15 Figure 1 is a cross-sectional view of a vacuum pumping arrangement shown schematically;

Figure 2 is an enlarged cross-sectional view of a portion of a regenerative pump of the arrangement shown in Figure 1;

Figure 3 is a diagram of a control system;

20 Figure 4 is a schematic representation of a vacuum pumping system;

Figure 5 is a schematic representation of another vacuum pumping system; and

Figures 6 to 8 are cross-sectional views of further vacuum pumping arrangements all shown schematically.

Referring to Figure 1, a vacuum pumping arrangement 10 is shown schematically, which comprises a molecular pumping mechanism 12 and a backing pumping mechanism 14. The molecular pumping mechanism comprises turbomolecular pumping means 16 and molecular drag, or friction, pumping means 18. Alternatively, the molecular pumping mechanism may comprise turbomolecular pumping means only or molecular drag pumping means only. The backing pump 14 comprises a regenerative pumping mechanism. A further drag pumping mechanism 20 may be associated with the regenerative pumping mechanism and provided between drag pumping mechanism 18 and regenerative pumping mechanism 14. Drag pumping mechanism 20 comprises three drag pumping stages in series, whereas drag pumping mechanism 18 comprises two drag pumping stages in parallel.

Vacuum pumping arrangement 10 comprises a housing, which is formed in three separate parts 22, 24, 26, and which houses the molecular pumping mechanism 12, drag pumping mechanism 20 and regenerative pumping mechanism 14. Parts 22 and 24 may form the inner surfaces of the molecular pumping mechanism 12 and the drag pumping mechanism 20, as shown. Part 26 may form the stator of the regenerative pumping mechanism 14.

Part 26 defines a counter-sunk recess 28 which receives a lubricated bearing 30 for supporting a drive shaft 32, the bearing 30 being at a first end

portion of the drive shaft associated with regenerative pumping mechanism 14. Bearing 30 may be a rolling bearing such as a ball bearing and may be lubricated, for instance with grease, because it is in a part of the pumping arrangement 10 distal from the inlet of the pumping arrangement. The inlet of the pumping arrangement may be in fluid connection with a semiconductor processing chamber in which a clean environment is required.

Drive shaft 32 is a common drive shaft to which both the molecular pumping mechanism 12 and backing pumping mechanism 14 are coupled and which is driven by motor 34 for rotating the molecular pumping mechanism 12 and backing pumping mechanism 14 at the same rotational speed.

The motor 34 is supported by parts 22 and 24 of the housing but may be supported at any convenient position in the vacuum pumping arrangement. In view of the common drive shaft 32, motor 34 is able to drive simultaneously the regenerative pumping mechanism 14, and the drag pumping mechanism 20 supported thereby, and also the molecular pumping mechanism 12. Generally, a regenerative pumping mechanism requires more power for operation than a molecular pumping mechanism, the regenerative pumping mechanism operating at pressures close to atmosphere where windage and air resistance is relatively high. A molecular pumping mechanism requires relatively less power for operation, and therefore, a motor selected for powering a regenerative pumping mechanism is also generally suitable for powering a molecular pumping mechanism. Means are provided for controlling the rotational speeds of the backing pumping mechanism and

the molecular pumping mechanism so that pressure in a chamber connected to, or operatively associated with, the arrangement can be controlled. A suitable control system diagram for controlling speed of the motor 34 is shown in Figure 3 and includes a pressure gauge 35 for measuring pressure in a chamber 33, and a controller 37 connected to the pressure gauge for controlling the pump's rotational speed.

Regenerative pumping mechanism 14 comprises a stator comprising a plurality of circumferential pumping channels disposed concentrically about a longitudinal axis A of the drive shaft 32 and a rotor comprising a plurality of arrays of rotor blades extending axially into respective said circumferential pumping channels. More specifically, regenerative pumping mechanism 14 comprises a rotor fixed relative to drive shaft 32. The regenerative pumping mechanism 14 comprises three pumping stages, and for each stage, a circumferential array of rotor blades 38 extends substantially orthogonally from one surface of the rotor body 36. The rotor blades 38 of the three arrays extend axially into respective circumferential pumping channels 40 disposed concentrically in part 26 which constitutes the stator of the regenerative pumping mechanism 14. During operation, drive shaft 32 rotates rotor body 36 which causes the rotor blades 38 to travel along the pumping channels, pumping gas from inlet 42 in sequence along the radially outer pumping channel, radially middle pumping channel and radially inner pumping channel where it is exhausted from pumping mechanism 14 via exhaust 44 at pressures close to or at atmospheric pressure.



An enlarged cross-section of a single stage of the regenerative pumping mechanism is shown in Figure 2. For efficient operation of the regenerative pumping mechanism 14, it is important that the radial clearance "C" between rotor blades 38 and stator 26 is closely controlled, and preferably kept to no more than 200 microns or less, and preferably less than 80 microns, during operation. An increase in clearance "C" would lead to significant seepage of gas out of pumping channel 40 and reduce efficiency of regenerative pumping mechanism 14. Therefore, regenerative pumping mechanism 14 is associated with the lubricated rolling bearing 30 which substantially resists radial movement of the drive shaft 32 and hence rotor body 36. However, if there is radial movement of the drive shaft at an end thereof distal from the lubricated bearing 30, this may also cause radial movement of the rotor of the regenerative pumping mechanism, resulting in loss of efficiency. In other words, bearing 30 may act as a pivot about which some radial movement may take place. To avoid loss of efficiency, the rotor 36 of the regenerative pumping mechanism is connected to the drive shaft 32 so as to be sufficiently close to the lubricated bearing 30 (i.e. the pivot) so that radial movement of the drive shaft translates substantially to axial movement of the rotor blades relative to respective circumferential pumping channels 40. Preferably, the bearing 30 is substantially axially aligned with the circumferential pumping channels so that any radial movement of the rotor blades 38 does not cause significant seepage. As shown, the stator 26 of the regenerative pumping mechanism 14 defines the recess for the bearing 30 and

the rotor body 36 is, as it will be appreciated, adjacent the stator 26. Accordingly, the bearing 30, which resists radial movement, prevents significant radial movement of the rotor body 36 and also hence of the rotor blades 38. Therefore, clearance "C" between the rotor blades 38 and stator 26  
5 can be kept within tolerable limits.

Extending orthogonally from the rotor body 36 are two cylindrical drag cylinders 46 which together form rotors of drag pumping mechanism 20. The drag cylinders 46 are made from carbon fibre reinforced material which is both strong and light. The reduction in mass when using carbon fibre drag  
10 cylinders, as compared with the use of aluminium drag cylinders, produces less inertia when the drag pumping mechanism is in operation. Accordingly, the rotational speed of the drag pumping mechanism is easier to control.

The drag pumping mechanism 20 shown schematically is a Holweck  
~~type drag pumping mechanism in which stator portions 48 define a spiral~~  
15 channel between the inner surface of housing part 24 and the drag cylinders 46. Three drag stages are shown, each of which provides a spiral path for gas flow between the rotor and the stator. The operation and structure of a Holweck drag pumping mechanism is well known. The gas flow follows a tortuous path flowing consecutively through the drag stages in series.

20 The molecular pumping mechanism 12 is driven at a distal end of drive shaft 32 from the regenerative pumping mechanism 14. A back up bearing may be provided to resist extreme radial movement of the drive shaft 32 during, for instance, power failure. As shown, the lubricant free bearing is

a magnetic bearing 54 provided between rotor body 52 and a cylindrical portion 56 fixed relative to the housing 22. A passive magnetic bearing is shown in which like poles of a magnet repel each other resisting excessive radial movement of rotor body 52 relative to the central axis A. In practice, the drive shaft may move about 0.1 mm.

A small amount of radial movement of the rotor of a molecular pumping mechanism does not significantly affect the pumping mechanism's performance. However, if it is desired to further resist radial movement, an active magnetic bearing may be adopted. In an active magnetic bearing, electro magnets are used rather than permanent magnets in passive magnetic bearings. Further provided is a detection means for detecting radial movement and for controlling the magnetic field to resist the radial movement. Figures 6 to 8 show an active magnetic bearing.

A circumferential array of angled rotor blades 58 extend radially outwardly from rotor body 52. At approximately half way along the rotor blades 58 at a radially intermediate portion of the array, a cylindrical support ring 60 is provided, to which is connected drag cylinder 62 of drag pumping mechanism 18. Drag pumping mechanism 18 comprises two drag stages in parallel with a single drag cylinder 62, which may be made from carbon fibre to reduce inertia. Each of the stages is comprised of stator portions 64 forming with the tapered inner walls 66 of the housing 22 a spiral molecular gas flow channel. An outlet 68 is provided to exhaust gas from the drag pumping mechanism 18.

During normal operation, inlet 70 of pump arrangement 10 is connected to a chamber, the pressure of which it is desired to reduce. Motor 34 rotates drive shaft 32 which in turn drives rotor body 36 and rotor body 52. Gas in molecular flow conditions is drawn in through inlet 70 to the  
5 turbomolecular pumping means 16 which urges molecules into the molecular drag pumping means 18 along both parallel drag pumping stages and through outlet 68. Gas is then drawn through the three stages in series of the drag pumping mechanism 20 and into the regenerative pumping mechanism through inlet 42. Gas is exhausted at atmospheric pressure or thereabouts  
10 through exhaust port 44.

Regenerative pumping mechanism 14 is required to exhaust gas at approximately atmospheric pressure. Accordingly, the gas resistance to passage of the rotor blades 38 is considerable and therefore the power and torque characteristics of motor 34 must be selected to meet the requirements  
15 of the regenerative pumping mechanism 14. The resistance to rotation encountered by the molecular pumping mechanism 12 is relatively little, since the molecular pumping mechanism operates at relatively low pressures. Furthermore, the structure of the drag pumping mechanism 18 with its only moving part being a cylinder rotated about axis A does not suffer significantly  
20 from gas resistance to rotation. Therefore, once power and torque characteristics for motor 34 have been selected for regenerative pumping mechanism 14, only a relatively small proportion of extra capacity is needed so that the motor also meets the requirements of molecular pumping

mechanism 12. In other words, a 200w motor, which is typically used for a molecular pumping mechanism, is significantly less powerful than motor 34 which preferably is a 2kw motor. In the prior art, the typical motor is not sufficiently powerful for pressure change in a chamber to be controlled by  
5 controlling the rotational speed of the pump. However, since a powerful motor is selected to drive regenerative pumping mechanism 14, the additional power can also be used to control rotational speed of the molecular pumping mechanism and thereby control pressure.

A typical turbomolecular pumping means is evacuated to relatively  
10 low pressures before it is started up. In the prior art, a backing pumping mechanism is used for this purpose. Since the backing pumping mechanism and turbomolecular pumping means are associated with the same drive shaft in vacuum pumping arrangement 10, this start up procedure is not possible. Accordingly, ~~the vacuum pumping arrangement forms part of a vacuum~~  
15 pumping system which comprises additional evacuation means to evacuate at least the turbomolecular pumping means 16 prior to start up to a predetermined pressure. Preferably, the turbomolecular pumping means is evacuated to less than 500 mbar prior to start up. Conveniently, the whole vacuum pumping arrangement is evacuated prior to start up, as shown in  
20 Figures 4 and 5. The evacuation means may be provided by an additional pump, although this is not preferred since an additional pump would increase costs of the system. When the pumping arrangement 10 is used as part of a semi-conductor processing system, it is convenient to make use of a pump or

pumping means associated with the system such as the pump for the load lock chamber. Figure 4 shows the arrangement of a semiconductor processing system, in which the load lock pump 74 is, in normal use, used to evacuate pressure from load lock chamber 76. A valve 78 is provided between load  
5 lock chamber 76 and load lock pump 74. Load lock pump 74 is connected to the exhaust of pumping arrangement 10 via valve 80. A further valve 82 is provided downstream of exhaust 44 of pumping arrangement 10. During start up, valve 78 and valve 82 are closed whilst valve 80 is opened. Load lock pump 74 is operated to evacuate gas from arrangement 10 and therefore from  
10 turbomolecular pumping means 16. During normal operation, valves 82 and 78 are opened whilst valve 80 is closed. Arrangement 10 is operated to evacuate pressure from vacuum chamber 84.

Alternatively, vacuum pumping arrangement 10 can be started up as described with reference to Figure 5. The additional evacuation means  
15 comprises a high pressure nitrogen supply which is connected to an ejector pump 90 via valve 88. Valve 88 is opened so that high pressure nitrogen is ejected to evacuate arrangement 10 and therefore turbomolecular pumping means 16. Nitrogen is a relatively inert gas and does not contaminate the system.

20 Although the pumping arrangement 10 may be evacuated prior to start up, it is also possible to evacuate the arrangement after start up, since the arrangement can be started but will not reach suitable rotational speeds until evacuation is performed.

There now follows a description of three further embodiments of the present invention. For brevity, the further embodiments will be discussed only in relation to the parts thereof which are different to the first embodiment and like reference numerals will be used for like parts.

5           Figure 6 shows a vacuum pumping arrangement 100 comprising an active magnetic bearing in which a cylindrical pole of the magnetic bearing 54 is mounted to the drive shaft 32 with a like pole being positioned on housing 22. The rotor body 52 of the turbomolecular pumping means 16 of the molecular pumping mechanism, is disc-shaped and the overall size of the  
10 arrangement 100 is reduced as compared with the first embodiment.

In Figure 7, a vacuum pumping arrangement 200 is shown in which the turbomolecular pumping means 12 comprises two turbomolecular pumping stages 16. A stator 92 extends radially inwardly from housing part 22 between the two turbo stages 16.

15           In Figure 8, a vacuum pumping arrangement 300 is shown in which molecular drag pumping mechanism 20 has been omitted.

CLAIMS

1. A vacuum pumping arrangement for controlling pressure in a chamber, the arrangement comprising a molecular pumping mechanism and a backing  
5 pumping mechanism, said backing pumping mechanism being rotatable by a motor, said motor being arranged to rotate said molecular pumping mechanism simultaneously with said backing pumping mechanism, and means for controlling the rotational speeds of the backing pumping mechanism and the molecular pumping mechanism.

10

2. A vacuum pumping arrangement as claimed in claim 1, wherein the molecular pumping mechanism and the backing pumping mechanism are arranged to be driven by a common drive shaft which is arranged to be driven  
by said motor.

15

3. A vacuum pumping arrangement as claimed in claim 1 or 2, wherein said molecular pumping mechanism comprises molecular drag pumping means.

20

4. A vacuum pumping arrangement as claimed in claim 3, wherein said molecular drag pumping means comprises Holweck pumping means.



5. A vacuum pumping arrangement as claimed in claim 4, wherein a holweck cylinder of the Holweck pumping means is formed from carbon fibre reinforced material.

5 6. A vacuum pumping arrangement as claimed in any one of the preceding claims, said molecular pumping mechanism comprising turbomolecular pumping means.

7. A vacuum pumping arrangement as claimed in any one of the  
10 preceding claims, wherein the backing pumping mechanism is a regenerative pumping mechanism.

8. A vacuum pumping arrangement as claimed in any one of the  
preceding claims, wherein the control means comprises means for measuring  
15 the pressure in the chamber, and means for changing the rotational speeds of the mechanisms in dependence on the measured pressure.

9. A method of controlling pressure in a chamber connected to an inlet of a vacuum pumping arrangement comprising a backing pumping mechanism  
20 and a molecular pumping mechanism, and a motor for driving said backing pumping mechanism, the method comprising using said motor to control rotation of said molecular pumping mechanism thereby to control pressure in said chamber.

10. A method as claimed in claim 9, wherein the backing pumping mechanism and the molecular pumping mechanism are coupled to a common drive shaft and the method comprises using the motor to control rotation of  
5 the common drive shaft thereby to control pressure in said chamber.

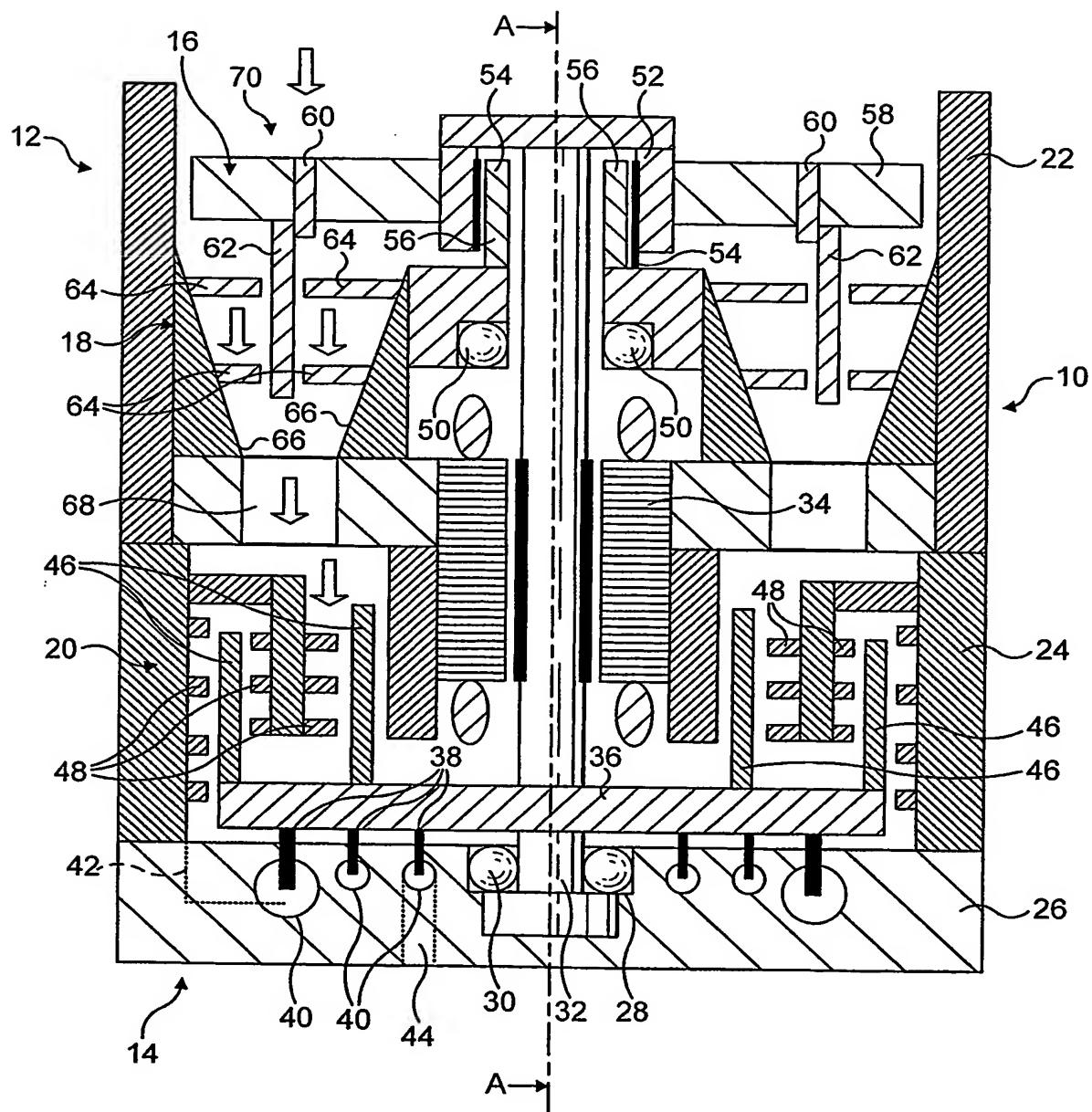


FIG. 1

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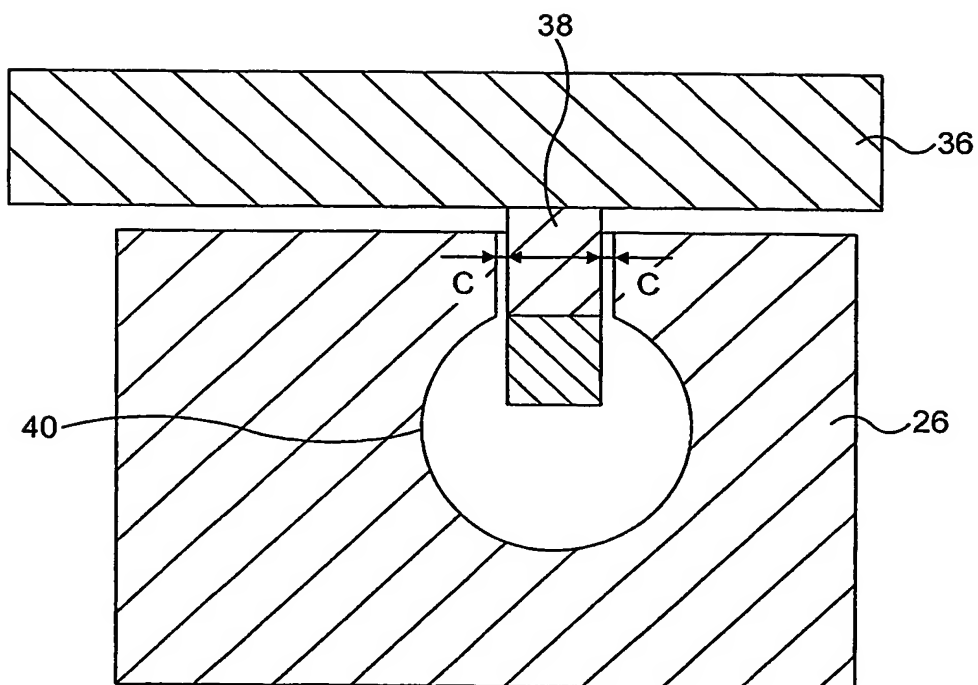


FIG. 2

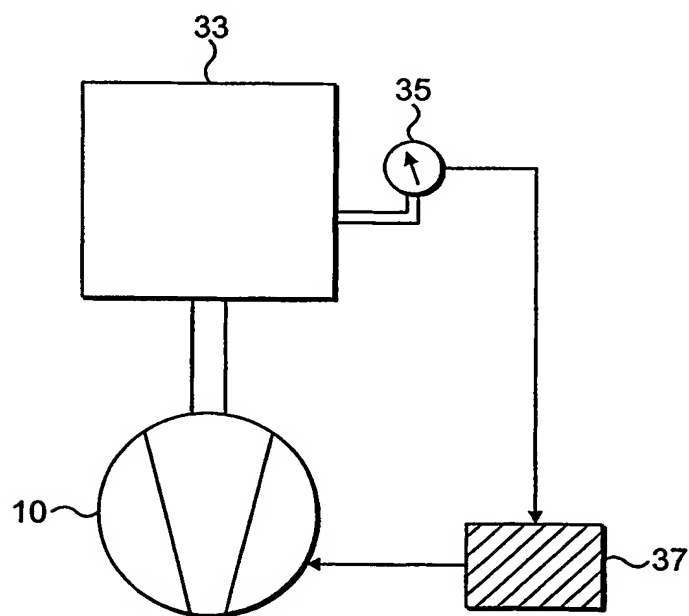


FIG. 3

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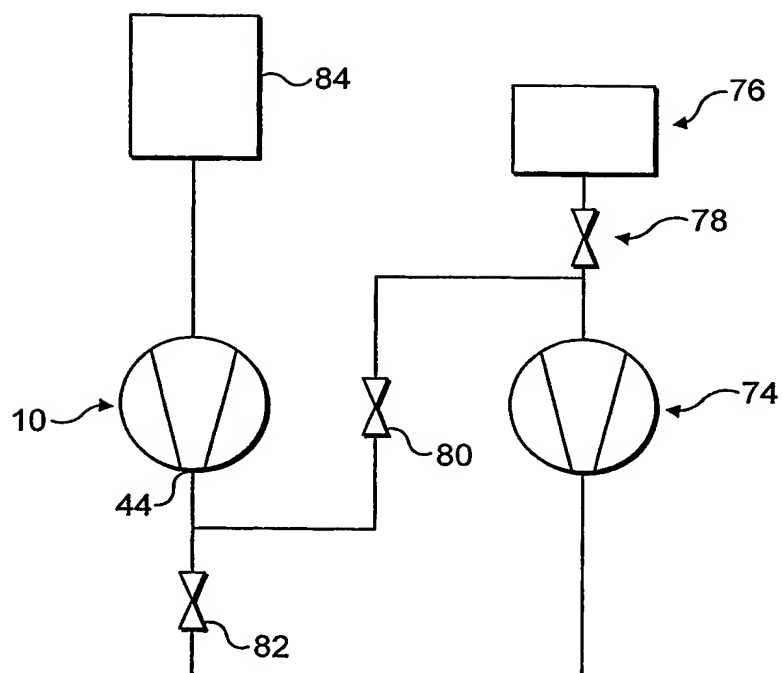


FIG. 4

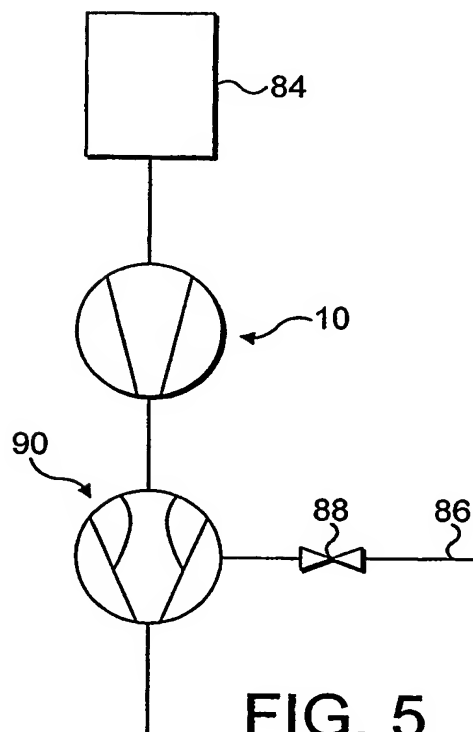
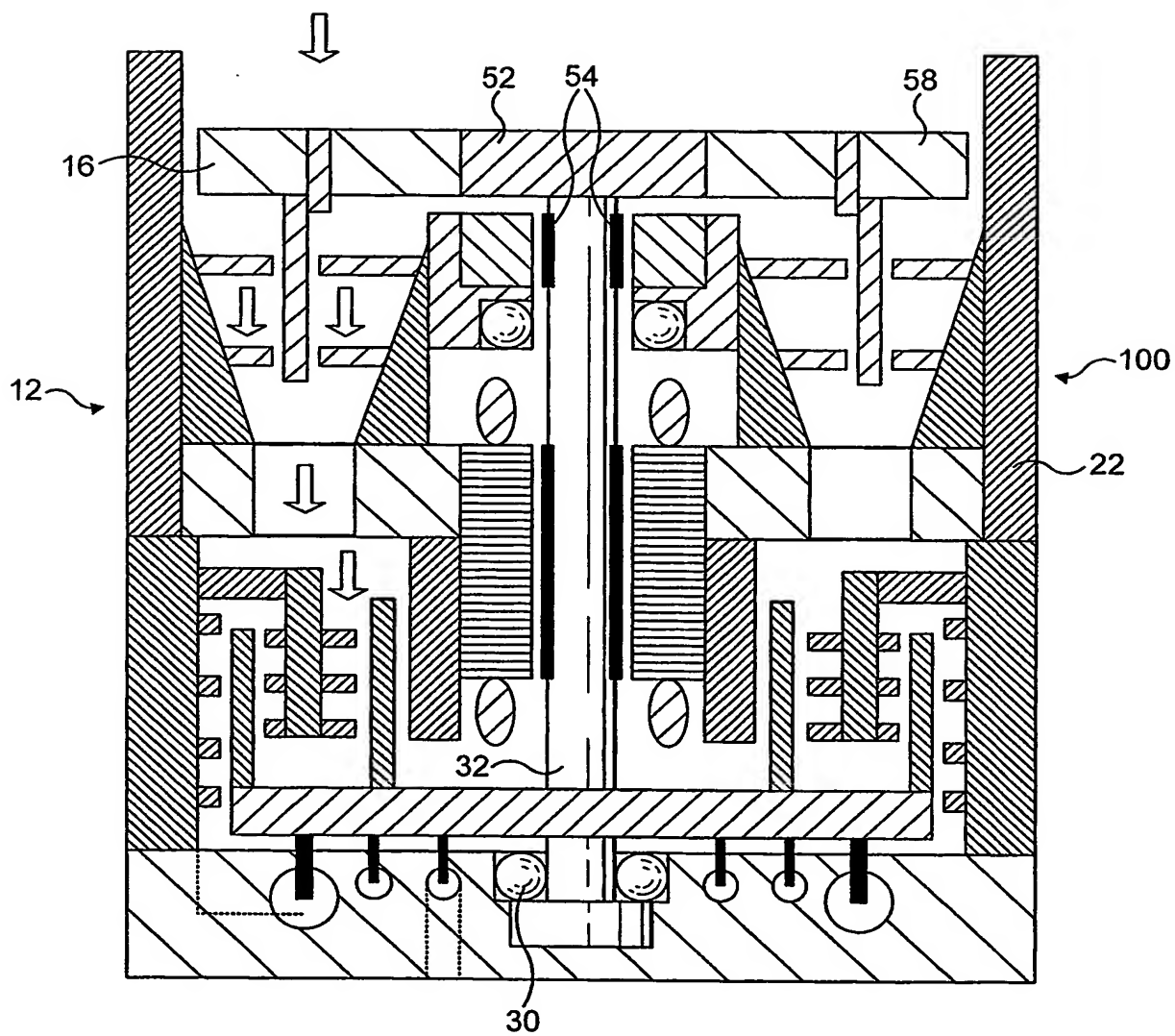


FIG. 5





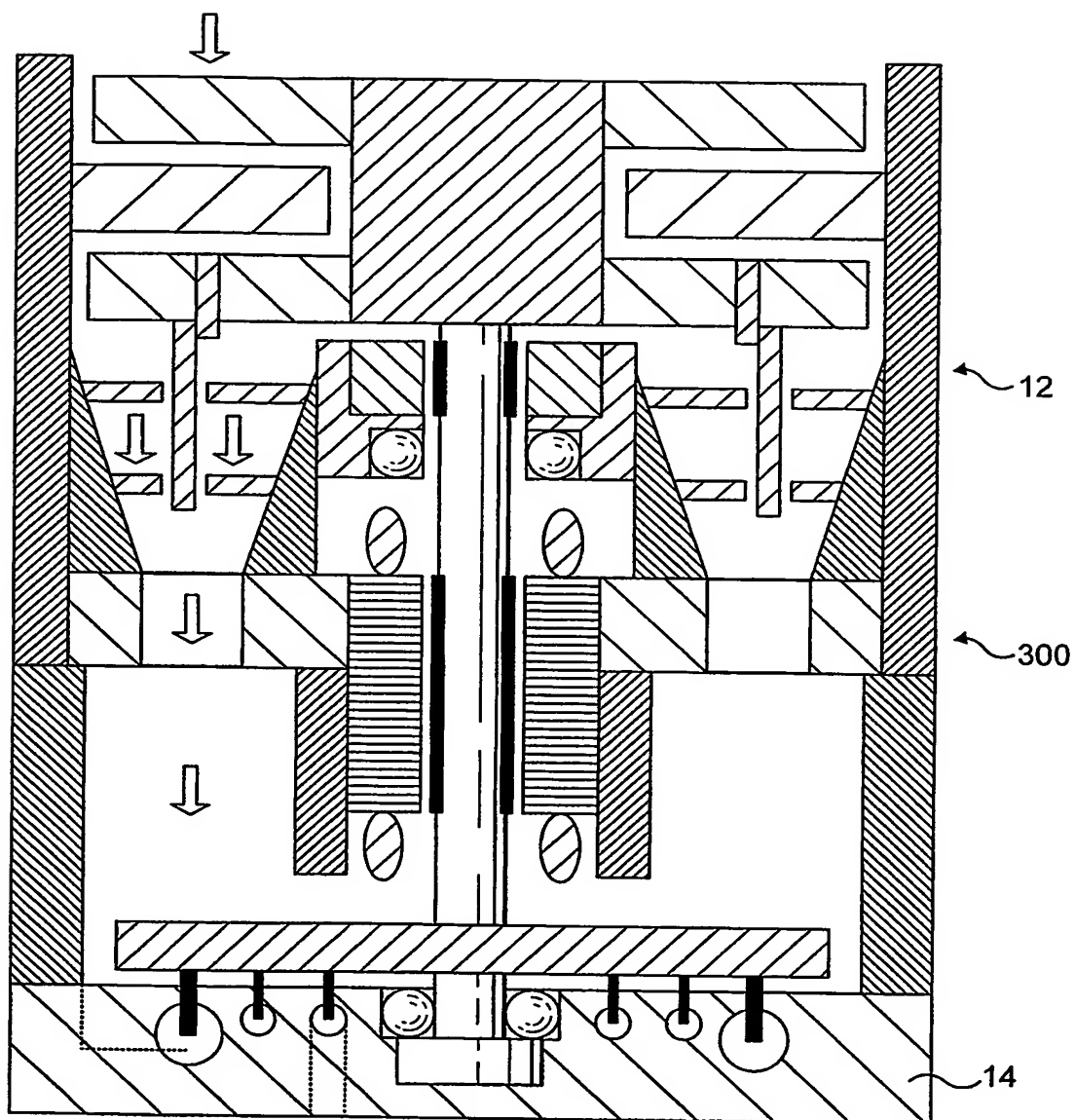


FIG. 8



# INTERNATIONAL SEARCH REPORT

Inventor Application No  
PCT/GB 03/05377

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 7 F04D27/02 F04D19/04

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 F04D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 1 213 482 A (SEIKO INSTR INC) 12 June 2002 (2002-06-12) column 3, line 28 -column 4, line 40 column 5, line 30 - line 43; figures 1-3 ----	1,3,4,6, 8,9
Y	EP 0 900 940 A (EBARA CORP) 10 March 1999 (1999-03-10) column 3, line 27 -column 5, line 17; figures 1-2B ----	1-3,6-10
Y	EP 1 234 982 A (VARIAN SPA) 28 August 2002 (2002-08-28) column 2, line 56 -column 3, line 51; figures 1-3 ----- -/-	1-3,6-10

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

24 March 2004

Date of mailing of the international search report

31/03/2004

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## INTERNATIONAL SEARCH REPORT

Automatic Application No  
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## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	EP 0 340 685 A (NIPPON FERROFLUIDICS KK) 8 November 1989 (1989-11-08) column 2, line 11 - column 3, line 24; figure 1	1,3,4,6, 9
Y	EP 1 081 380 A (EBARA CORP) 7 March 2001 (2001-03-07) column 4, line 29 - line 57; figure 1	1,3,4,6, 9
A	US 3 616 680 A (SCHRADER WILHELM F) 2 November 1971 (1971-11-02) column 5, line 46 - line 51	1
A	EP 0 226 039 A (HITACHI LTD) 24 June 1987 (1987-06-24)	

# INTERNATIONAL SEARCH REPORT

Information on patent family members

Application No

PCT/GB 03/05377

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
EP 1213482	A	12-06-2002	JP 2002168192 A EP 1213482 A1 US 2002098092 A1	14-06-2002 12-06-2002 25-07-2002
EP 0900940	A	10-03-1999	JP 11082347 A DE 69820938 D1 EP 0900940 A2 US 6088508 A	26-03-1999 12-02-2004 10-03-1999 11-07-2000
EP 1234982	A	28-08-2002	EP 1234982 A1 DE 60101368 D1	28-08-2002 15-01-2004
EP 0340685	A	08-11-1989	JP 1277698 A DE 68914320 D1 DE 68914320 T2 EP 0340685 A2 US 5092740 A	08-11-1989 11-05-1994 21-07-1994 08-11-1989 03-03-1992
EP 1081380	A	07-03-2001	JP 2000038999 A EP 1081380 A1 US 6474949 B1 WO 9960272 A1 TW 483988 B	08-02-2000 07-03-2001 05-11-2002 25-11-1999 21-04-2002
US 3616680	A	02-11-1971	BE 757352 A1 CA 922584 A1 CH 519137 A DE 2049117 A1 FR 2066532 A5 GB 1330685 A JP 51025158 B NL 7015084 A	16-03-1971 13-03-1973 15-02-1972 06-05-1971 06-08-1971 19-09-1973 29-07-1976 29-04-1971
EP 0226039	A	24-06-1987	JP 62113887 A EP 0226039 A1	25-05-1987 24-06-1987